

CODES:

FLORIDA BUILDING CODE 2014, 5TH EDITION
ASCE STANDARD 7-2010
MIAMI DADE WIND SPEED = 175 MPH

WIND DESIGN REQUIREMENTS:

ULTIMATE DESIGN WIND SPEED, Vult (3 sec. gust) 175 mph
NOMINAL DESIGN WIND SPEED, Vasd 135 mph

RISK CATEGORY II
HEIGHT TO CENTROID 15 FT max.
EXPOSURE CATEGORY D
ENCLOSURE CATEGORY N/A
EFFECTIVE WIND AREA N/A

INTERNAL PRESSURE COEFFICIENT GCpI N/A
DIRECTIONALITY FACTOR Kd 0.90
TOPOGRAPHIC FACTOR Kzt 1.00
GUST EFFECT FACTOR N/A

WIND LOAD METHOD:

VELOCITY PRESSURE:
based on ASCE 7-10, Eq. 29.3-1
 $q_z = 0.00256 K_z K_{zt} K_d V^2$ psf
 $K_z = 1.03$
 $V = V_{ult}$
 $q_z = 72.7$ psf

WIND PRESSURES:
based on ASCE 7-10 Eq. 29.5.1 & FBC 1620.6
 $F = q_h GCr Af$ psf Eq. 29.5-2
GCr = 1.1 FOR LATERAL FORCES
GCr = 1.0 FOR VERTICAL FORCES

LOAD COMBINATIONS:

POSITIVE VERTICAL FORCE: $1.0 \cdot D + 0.6 \cdot W$ [FBC 1605.3.1 EQ. 16-12]
SLIDING & ANCHOR PULLOUT: $0.6 \cdot D + 0.6 \cdot W$ [FBC 1605.3.1 EQ. 16-15]
OVERTURNING: $0.67 \cdot D + 0.78 \cdot W$ [FBC 1605.3.2 EQ. 16-18]

GENERAL NOTES:

- THIS ENGINEERING REPORT DOCUMENTS THE ANALYSIS OF AC EQUIPMENT MOUNTED ON A CONCRETE FOUNDATION PAD AND THE ASSOCIATED ANCHORING SYSTEMS TO RESIST DEAD WEIGHT AND WIND LOAD FORCES.
- THE ANALYSIS CONFORMS TO THE REQUIREMENTS OF THE FLORIDA BUILDING CODE 2014 AND ASCE 7-2010, FOR USE WITHIN & OUTSIDE HVHZ.
- THE AC UNIT IS MOUNTED ON A CONCRETE FOUNDATION PAD. THE CONCRETE FOUNDATION PAD SHALL BE MIN. 10" THICK AT ANCHOR LOCATIONS.
- THE ANCHORAGE IS DESIGNED AND VERIFIED BY STRUCTURAL ANALYSIS BY THIS ENGINEER.
- ALTERNATE DESIGNS FOR SUPPORTS WITHIN 15' OF GROUND LEVEL, THAT ARE DESIGNED TO RESIST THE ABOVE WIND LOADS MAY BE USED AT THE CONTRACTOR'S OPTION. FOR ALTERNATE DESIGNS FOR SUPPORTS WITHIN 15' OF GROUND LEVEL, PROVIDE DETAILS AND CALCULATIONS SIMILAR TO THIS SHEET AND DETAILED CALCULATIONS ON SHEET 2, STAMPED BY A PROFESSIONAL ENGINEER REGISTERED IN THE STATE OF FLORIDA.
- THE CONTRACTOR IS RESPONSIBLE FOR SAFETY, INSTALLATION, AND SPECIAL INSPECTIONS & TESTS PER FBC CHAPTER 17.

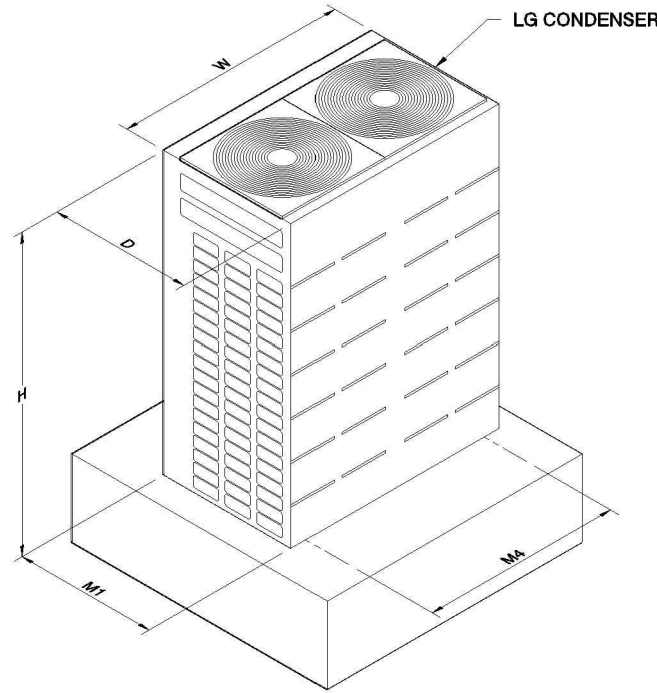
CALCULATIONS: SEE DETAILED CALCULATIONS ON SHEET 2.

WIND LATERAL AND VERTICAL FORCES:

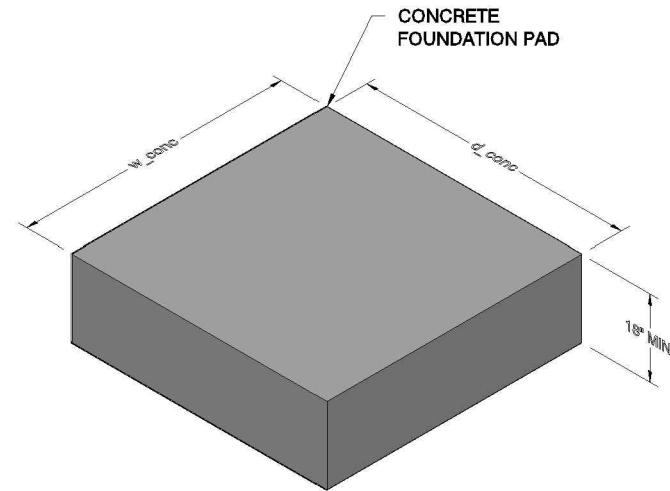
- THE WIND LOAD ACTING NORMAL TO THE LARGE VERTICAL SIDE OF THE AC UNIT IS USED FOR WORST CASE SHEAR.
- THE WIND LOAD ACTING ON THE TOP OF THE UNIT UPWARD AND THE HORIZONTAL WIND LOAD ARE USED TO CALCULATE UPLIFT AND MOMENT.
- THESE FORCES MUST BE RESISTED BY THE SHEAR AND TENSILE STRENGTHS OF THE ANCHORS HOLDING THE UNIT TO THE CONCRETE FOUNDATION. THE ANCHORAGES & MOUNTING ARE VERIFIED BY THIS ENGINEER TO BE WITHIN THE ALLOWABLE STRENGTHS OF ITS ELEMENTS AND CONNECTIONS.

ENCLOSURE FASTENERS:

- THE METAL SHELL FASTENERS MUST RESIST THE NEGATIVE WIND PRESSURES CAUSING TENSILE STRESS IN THE SCREWS AND PULL-OVER EFFECTS OF THE SHEET METAL.



GROUND MOUNT CONFIGURATION



CONCRETE PAD W/ TURNDOWN EDGE

| CONCRETE FOUNDATION PAD STRENGTH LIMITS | | |
|---|--------|-------|
| LIMIT TYPE | AMOUNT | UNITS |
| MAX SHEAR AT ANCHOR | 0.310 | KIP |
| MAX PULLOUT AT ANCHOR | 1.090 | KIP |

FOUNDATION NOTES:

- FOUNDATION IS DESIGNED AND VERIFIED FOR THE FORCES DESCRIBED IN THIS DOCUMENT AS SUMMARIZED IN THE ENGINEERING CALCULATIONS INCLUDED.
- t_{conc} = FOUNDATION SLAB THICKNESS = 10" MIN.
- FOUNDATION HEIGHT AT EDGES = 18" MIN.
- FOUNDATION SHALL EXTEND MIN. 12" BELOW GROUND.
- w_{conc} = FOUNDATION WIDTH = 60" MIN, 72" MAX.
- d_{conc} = FOUNDATION DEPTH = 60" MIN, 72" MAX.
- TOP OF FOUNDATION PAD SHALL BE MIN. 4" ABOVE ADJACENT GRADE.
- AC UNIT MUST BE CENTERED ON FOUNDATION.
- AC UNIT IS ANCHORED TO CONCRETE SLAB W/ GALV 3/8" Ø HILTI KWIK BOLT 3 ANCHORS WITH MIN. 2" EMBED. IN CONCRETE. EACH ANCHOR CAPACITY IS COMBINED TENSION = 1090 LBS AND SHEAR = 310 LBS.
- MIN. REINFORCEMENT SHALL BE ONE LAYER OF #4 BARS @ 14" EACH WAY, CENTERED IN THE CONCRETE.
- FOUNDATION SUBGRADE SHALL BE COMPACTED TO PROVIDE MIN. 1200 PSF ALLOWABLE BEARING PRESSURE.

OTHER NOTES:

- 1"± NON-METALLIC NON-SHRINK GROUT MAY BE USED UNDER THE MOUNTING PLATES.

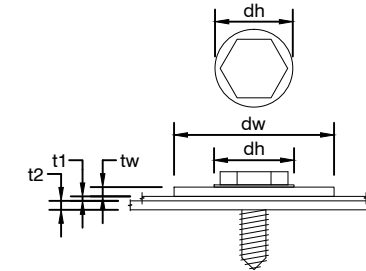
ENGINEERING CONFORMANCE ANALYSIS:

THE TABLE BELOW SHOWS DIMENSIONS, MIN FOUNDATION DEPTH & WIDTH, AND SHELL ENCLOSURE SCREWS FOR SOME MODELS OF LG ELECTRONICS USA HVAC OUTDOOR EQUIPMENT THAT MEET THE FOLLOWING ANALYSIS:

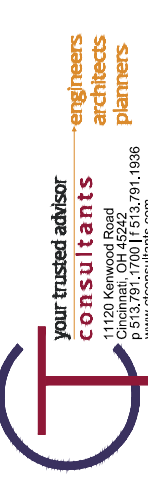
- FOUNDATION STRENGTH: STRENGTH TO RESIST UNIT WEIGHT AND WIND LOADS ON LATERAL AND VERTICAL SURFACES
- ANCHORS: PULLOUT AND SHEAR DUE TO OVERTURNING AND SLIDING FORCE IS WITHIN REQUIREMENTS
- EQUIPMENT METAL COVER FASTENERS: MIN NUMBER AND SIZE

| MODEL # | CONDENSER DIMENSIONS | | | | | | CONCRETE PAD | | SHELL SCREWS | ANCHOR STRENGTH | | DESIGN CHECK W/ NOM/REQ'D >= 1.00 = OK |
|--|----------------------|-------|-------|-------|-------|-----|--------------|------------|---------------------------|-----------------|--------|--|
| | W | D | H | M1 | M4 | Wt | MIN d_conc | MIN w_conc | ON LONG SIDE, QTY. & SIZE | SHEAR | UPLIFT | |
| ARUB096BTE4 ARUB096DTE4 ARUN096BTE4 ARUN096DTE4 ARUB121BTE4 ARUB121DTE4 ARUN121BTE4 ARUN121DTE4 | 48.81 | 29.94 | 66.13 | 29.06 | 43.38 | 563 | 60 | 60 | 18, #10 | 0.87 | 0.78 | 0.35 |
| ARUN122BTE4 ARUN122DTE4 ARUB122BTE4 ARUB122DTE4 | 48.81 | 29.94 | 66.13 | 29.06 | 43.38 | 661 | 60 | 60 | 18, #10 | 0.87 | 0.76 | 0.35 |
| ARUN144BTE4 ARUN144DTE4 ARUB144BTE4 ARUB144DTE4 ARUN168BTE4 ARUN168DTE4 ARUB168BTE4 ARUB168DTE4 | 48.81 | 29.94 | 66.13 | 29.06 | 43.38 | 628 | 60 | 60 | 18, #10 | 0.87 | 0.77 | 0.35 |
| ARUN145BTE4 ARUN145DTE4 ARUB145BTE4 ARUB145DTE4 ARUN169BTE4 ARUN169DTE4 ARUB169BTE4 ARUB169DTE4 | 48.81 | 29.94 | 66.13 | 29.06 | 43.38 | 660 | 60 | 60 | 18, #10 | 0.87 | 0.76 | 0.35 |

NOTE: THE CONCRETE PAD DIMENSIONS ARE MINIMUMS. CONCRETE PAD MAY BE BUILT TO SUPPORT MORE THAN ONE CONDENSER UNIT AS OUTLINED IN THE LG ELECTRONICS USA INSTALLATION MANUAL.



| ENCLOSURE FASTENERS | | |
|-----------------------------------|-------|-------|
| DESCRIPTION | SIZE | UNITS |
| SCREW SIZE (d) | #10 | |
| INTEGRAL WASHER SIZE (dw) | 0.50 | IN |
| THICKNESS OF SHEET METAL (t1) | 0.043 | IN |
| MIN. THICKNESS OF FRAME (t2) | 0.07 | IN |
| DEPTH OF PENETRATION | 0.25 | IN |
| SCREW YIELD STRENGTH | 55 | KSI |
| ALLOWABLE TENSILE STRENGTH/SCREW | 321 | LBS |
| ALLOWABLE PULLOVER STRENGTH/SCREW | 371 | LBS |
| ALLOWABLE PULL-OUT STRENGTH/SCREW | 170 | LBS |



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31626

48-30-G-73 INFORMATION & DIAGRAMS
LG ELECTRONICS USA HVAC
OUTDOOR CONDENSING UNIT
GROUND MOUNT CONFIGURATION

| NO. | DATE | DESCRIPTION | BY |
|-----|------|-------------|----|
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| SCALE | DATE |
| NTS | 10/28/16 |
| DRAWN BY | PROJECT MGR |
| JDP | PCP |
| PROJECT NO. | FLAT FILE |
| 160387 | |
| DRAWING NO. | 48-30-G-73 |
| SHEET | 1 OF 2 |

ENGINEERING CALCULATION DETAIL SHEET

Outdoor Condensor Units on Concrete Pad - Suitability Verification
 Designed by: Paul C. Perrin, PE, SE

DESIGN METHODOLOGY: ASD

OBJECTIVE:

Determine Wind Load on AC unit mounted on concrete foundation using ASCE 7 (2010), Section 29.5. Confirm stability, anchor configuration and strength, and equipment envelope fastening.

WIND LOAD: (See also "Wind Design Requirements" on Drawing 1)

Vult = 175 mph (FBC 2014 1620.2) for Miami-Dade, Risk Category II

From "29.3 Velocity Pressure"
 $q_z = 0.00256 * K_z * K_{zt} * K_d * V^2 = 72.7 \text{ psf}$ (Eq. 29.3-1)
 From "29.5 Design Wind Loads - Other Structures"
 $F = q_z * (G * C_r) * A_f$ (Eq. 29.5-1)

Fvertical = $72.7 \text{ psf} * (1.0) * A_f = 72.7 \text{ psf} * \text{Area} \text{ (ft}^2\text{)}$
 Flateral = $72.7 \text{ psf} * (1.1) * A_f = 79.9 \text{ psf} * \text{Area} \text{ (ft}^2\text{)}$

Example AC Unit:

Use ARUB096BTE4 in Table w/ dims (W, D, H, Wt) = (48.81", 29.94", 66.13", 563 lbs)

WIND LOAD FORCES:

Top Area = $29.94" * 48.81" / (144 \text{ in}^2/\text{ft}^2) = 10.15 \text{ sf}$
 Fw vertical (Fw_vert) = $72.7 \text{ psf} * 10.15 \text{ sf} = 738 \text{ lbs}$ (unfactored)

Long side Area = $48.81" * 66.13" / (144 \text{ in}^2/\text{ft}^2) = 22.42 \text{ sf}$
 Fw lateral (Fw_lat) = $79.9 \text{ psf} * 22.42 \text{ sf} = 1792 \text{ lbs}$ (unfactored)

LOAD COMBINATIONS:

0.67D + 0.78W for overturning FBC 1605.3.2 Eq. 16-18
 0.6D + 0.6W for sliding and anchors FBC 1605.3.1 Eq. 16-15

CALCULATE REACTION FORCES ON CONCRETE FOUNDATION:

Shear V1 = $0.6 * Fw_lat / 4 \text{ anchors} = 0.6 * 1792 \# / 4 = 269 \text{ lbs}$
 Pull-up R1 = $[0.78 * Fw_lat * H/2 + (0.78 * Fw_vert - 0.67 * Wt) * (M1/2)] / (M1) / 2 \text{ legs}$
 = $[0.78 * 1792 \# * (66.13"/2) + (0.78 * 738 \# - 0.67 * 563 \#) * (29.06"/2)] / (29.06") / 2$
 = 0.845 kips

SOIL BEARING PRESSURE AT CONCRETE FOUNDATION:

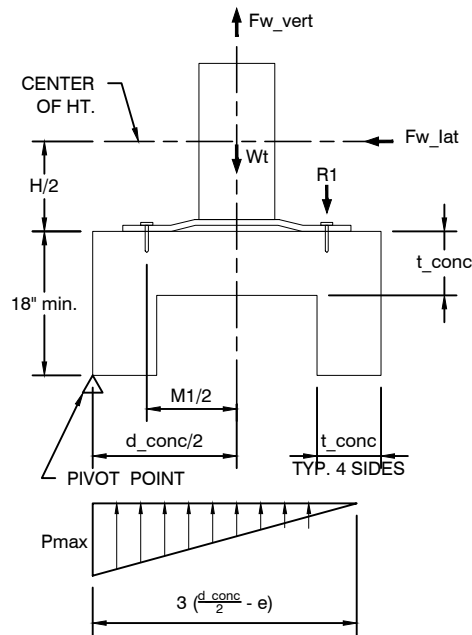
Wt conc = $150 \text{ pcf} * \{t_conc * w_conc * d_conc + (18" - t_conc) * 2 * t_conc * [w_conc + (d_conc - 2 * t_conc)]\}$
 = $150 \text{ pcf} * \{10" * 60" * 60" + (18" - 10") * 2 * 10" * [60" + (60" - 2 * 10")]\}$
 = 4.51 kips

P = $0.67 * (Wt + Wt_conc) - 0.78 * Fw_vert$
 = $0.67 * (0.563 \text{ kip} + 4.51 \text{ kip}) - 0.78 * 738 \#$
 = 2.826 kip

M_ot = $0.78 * Fw_lat * (18" + H/2)$
 = $0.78 * 1792 \# * (18" + 66.13"/2)$
 = 71.380 kip*in

e = $M_ot / P = 71.380 \text{ kip*in} / 2.826 \text{ kips} = 25.26"$

If $e = 25.26" > d_conc / 6 = 10.00"$
 then Pmax = $2P / [3 * w_conc * \{(d_conc / 2) - e\}]$
 = $2 * 2.826 \text{ kip} / [3 * 60" * \{(60"/2) - 25.26'\}]$
 = 953 psf



SINCE THIS DESIGN IS BASED ON WIND PRESSURE, qz, THIS DESIGN IS ALSO SUITABLE FOR THE FOLLOWING CASES:
 • ULTIMATE WIND SPEED = 186 MPH, EXPOSURE CATEGORY C, HEIGHT UP TO 15 FT.

DESIGN METHODOLOGY: ASD

VERIFY ANCHOR SHEAR RESISTANCE TO SLIDING:

Use Load Combination FBC 1605.3.1 Eq. 16-15
 $0.6D + 0.6W = 0.6 * Fw_lat = 0.6 * 1792 \# = 1075 \text{ lbs}$
 Shear per anchor = $1075 \# / 4 = 269 \text{ lbs}$
 Fsliding nominal = 0.310 kips
 Since 0.310 kips > 0.269 kips

Resistance to Sliding Checks OK.

CHECK OVERTURNING ANCHOR PULLOUT/UPLIFT RESISTANCE:

Use Load Combination FBC 1605.3.1 Eq. 16-15
 $0.6D + 0.6W$
 On one anchor
 Pull-up R1 = 0.845 kips
 Max uplift at one anchor = 1.090 kips
 Since 1.090 kips > 0.845 kips

Anchor Resistance to Overturning Checks OK.

CHECK SHEET METAL ENVELOPE FASTENER RESISTANCE:

Analysis based on AISI S100-2007 "Cold Formed Steel Structural Members" Section E4: Screw Connections
 Use Load Combination FBC 1605.3.1 Eq. 16-15
 $0.6D + 0.6W$
 On long side worst case
 $0.60 * Fw_lat = 0.60 * 1792 \# = 1075 \text{ lbs}$

Resistance to the metal shell pull-off is the minimum of the tensile strength of the screw and the pull-over strength of the sheet metal.

Inputs:
 #10 screw, d = 0.19" with integral 0.5"-diameter washer
 Thickness of metal shell, t1 = 0.043" (18 gauge)
 Depth of penetration of screw into frame, tc = 0.25"
 Strength of screw, Fu1 = 55 ksi

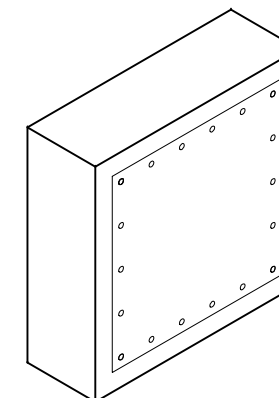
Based on the above data:

Allowable tensile of the screw, Pts/Omega = 321 lbs per screw (where Omega = 3.0)
 Allowable Pull-out strength, Pnot/Omega = 170 lbs per screw
 Allowable Pull-over strength, Pnov/Omega = 371 lbs per screw
 Therefore the min number of screws per long side = $1075 \# / 170 \#/\text{screw} = 6.32 \text{ screws}$
 Rounds up to min 7 screws per side, use 18 screws, spaced 12" O.C. minimum.

Anchor Resistance to Metal Enclosure Pull-Off Checks OK.

THE CALCULATIONS ON THE DRAWING ARE REPRESENTATIVE OF THE FOLLOWING LG ELECTRONICS OUTDOOR CONDENSING UNITS:

| | |
|-------------|-------------|
| ARUB096BTE4 | ARUN145DTE4 |
| ARUB096DTE4 | ARUB145BTE4 |
| ARUN096BTE4 | ARUB145DTE4 |
| ARUN096DTE4 | ARUN169BTE4 |
| ARUN121BTE4 | ARUN169DTE4 |
| ARUN121DTE4 | ARUB169BTE4 |
| ARUB121BTE4 | ARUB169DTE4 |
| ARUB121DTE4 | |
| ARUN122BTE4 | |
| ARUN122DTE4 | |
| ARUB122BTE4 | |
| ARUB122DTE4 | |
| ARUN144BTE4 | |
| ARUN144DTE4 | |
| ARUB144BTE4 | |
| ARUB144DTE4 | |
| ARUN168BTE4 | |
| ARUN168DTE4 | |
| ARUB168BTE4 | |
| ARUB168DTE4 | |
| ARUN145BTE4 | |



SCREW PATTERN

SCALE: NTS



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48-30-G-73 CALCULATIONS

LG ELECTRONICS USA HVAC
 OUTDOOR CONDENSING UNIT
 GROUND MOUNT CONFIGURATION

| NO. | DATE | REVISIONS | BY | DESCRIPTION |
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| JDP | PCP |
| PROJECT NO. | FLAT FILE |
| 160387 | |
| DRAWING NO. | |
| 48-30-G-73 | |
| SHEET 2 | OF 2 |