

**CODES:**

FLORIDA BUILDING CODE 2014, 5TH EDITION  
 ASCE STANDARD 7-2010  
 MIAMI DADE WIND SPEED = 186 MPH

**WIND DESIGN REQUIREMENTS:**

ULTIMATE DESIGN WIND SPEED,  $V_{ult}$  (3 sec. gust) 186 mph  
 NOMINAL DESIGN WIND SPEED,  $V_{asd}$  144 mph

RISK CATEGORY IV  
 HEIGHT TO CENTROID 63 FT  
 EXPOSURE CATEGORY D  
 ENCLOSURE CATEGORY N/A  
 EFFECTIVE WIND AREA N/A

INTERNAL PRESSURE COEFFICIENT  $GCP_i$  N/A  
 DIRECTIONALITY FACTOR  $K_d$  0.9  
 TOPOGRAPHIC FACTOR  $K_{zt}$  1.0  
 GUST EFFECT FACTOR N/A

**WIND LOAD METHOD:**

VELOCITY PRESSURE:  
 based on ASCE 7-10, Eq. 29.3-1  
 $q_z = 0.00256 K_z K_{zt} K_d V^2$  psf  
 $K_z = 1.32$   
 $V = V_{ult}$   
 $q_z = 105$  psf

WIND PRESSURES:  
 based on ASCE 7-10 Eq. 29.5.1 & FBC 1620.6  
 $F = q_h GCF Af$  psf Eq. 29.5-2  
 $GCF = 3.10$  FOR LATERAL FORCES  
 $GCF = 1.50$  FOR VERTICAL FORCES

**LOAD COMBINATIONS:**

POSITIVE VERTICAL FORCE:  $1.0 \cdot D + 0.6 \cdot W$  [FBC 1605.3.1 EQ. 16-12]  
 SLIDING & ANCHOR PULLOUT:  $0.6 \cdot D + 0.6 \cdot W$  [FBC 1605.3.1 EQ. 16-15]  
 OVERTURNING:  $0.67 \cdot D + 0.78 \cdot W$  [FBC 1605.3.2 EQ. 16-18]

**GENERAL NOTES:**

1. THIS ENGINEERING REPORT DOCUMENTS THE ANALYSIS OF AC EQUIPMENT MOUNTED ON A ROOF STAND AND THE ASSOCIATED ANCHORING SYSTEMS TO RESIST DEAD WEIGHT AND WIND LOAD FORCES.
2. THE ANALYSIS CONFORMS TO THE REQUIREMENTS OF THE FLORIDA BUILDING CODE 2014 AND ASCE 7-2010, FOR USE WITHIN & OUTSIDE HVHZ.
3. THE AC UNIT IS MOUNTED ON A METAL STAND WHICH IS SECURED TO THE ROOF.
4. ANCHORS USED TO FASTEN THE UNIT TO THE ROOF STAND ARE A307 OR HIGHER STRENGTH STEEL BOLTS.
5. THE ROOF STAND IS DESIGNED AND VERIFIED BY STRUCTURAL ANALYSIS BY THIS ENGINEER.
6. ALTERNATE ROOF STAND DESIGNS (E.G. ALUMINUM) THAT ARE DESIGNED TO RESIST THE ABOVE WIND LOADS MAY BE USED AT THE CONTRACTOR'S OPTION. FOR ALTERNATE ROOF STAND DESIGNS, PROVIDE DETAILS AND CALCULATIONS SIMILAR TO THIS SHEET AND DETAILED CALCULATIONS ON DRAWING 2, STAMPED BY A PROFESSIONAL ENGINEER REGISTERED IN THE STATE OF FLORIDA.
7. THE CONTRACTOR IS RESPONSIBLE FOR SAFETY, INSTALLATION, AND SPECIAL INSPECTIONS & TESTS PER FBC CHAPTER 17.

**CALCULATIONS:** SEE DETAILED CALCULATIONS ON DRAWING 2.

**WIND LATERAL AND VERTICAL FORCES:**

1. THE WIND LOAD ACTING NORMAL TO THE LARGE VERTICAL SIDE OF THE AC UNIT IS USED FOR WORST CASE SHEAR.
2. THE WIND LOAD ACTING ON THE TOP OF THE UNIT UPWARD AND THE HORIZONTAL WIND LOAD IS USED TO CALCULATE UPLIFT AND MOMENT.
3. THESE FORCES MUST BE RESISTED BY THE SHEAR AND TENSILE STRENGTHS OF THE ANCHORS HOLDING THE UNIT TO THE SUPPORT BAR AND ALSO THE ANCHORS HOLDING THE SUPPORT BAR TO THE ROOF STAND. THE ROOF STAND INTERNAL STRESSES ARE VERIFIED BY THIS ENGINEER TO BE WITHIN THE ALLOWABLE STRENGTHS OF ITS ELEMENTS AND CONNECTIONS.

**SUPPORT BAR STRENGTH:**

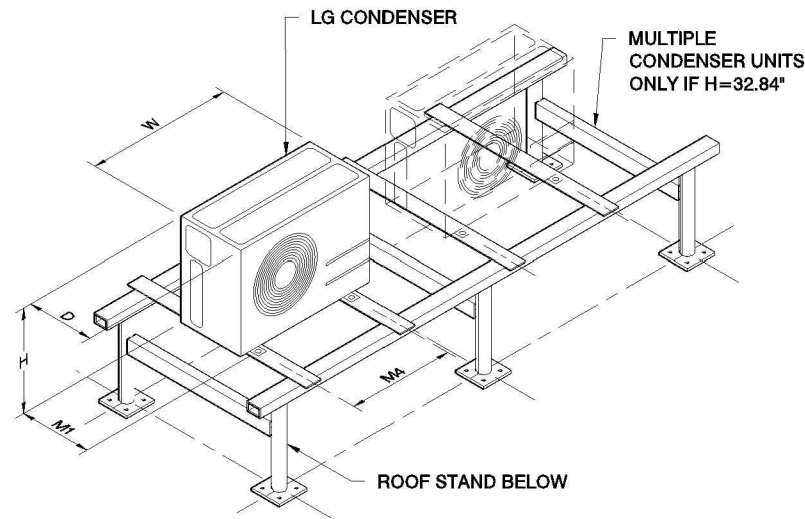
4. THE MOMENT AND SHEAR MUST BE TRANSFERRED FROM THE AC UNIT TO THE ROOF STAND BY A SUPPORT BAR AS THE AC UNIT DEPTH CAN BE UNEQUAL TO THE ROOF STAND DEPTH.
5. MAX MOMENT AND SHEAR TO THE SUPPORT BAR DETERMINE SELECTION OF THE SUPPORT BAR.

**ROOF STAND STRENGTH:**

6. CRITICAL LIMITS ARE THE POST LEGS AND WELD STRENGTH TO THE BASE, CROSS BRACE TO POST CONNECTION, AND RAILING TO POST CONNECTION.

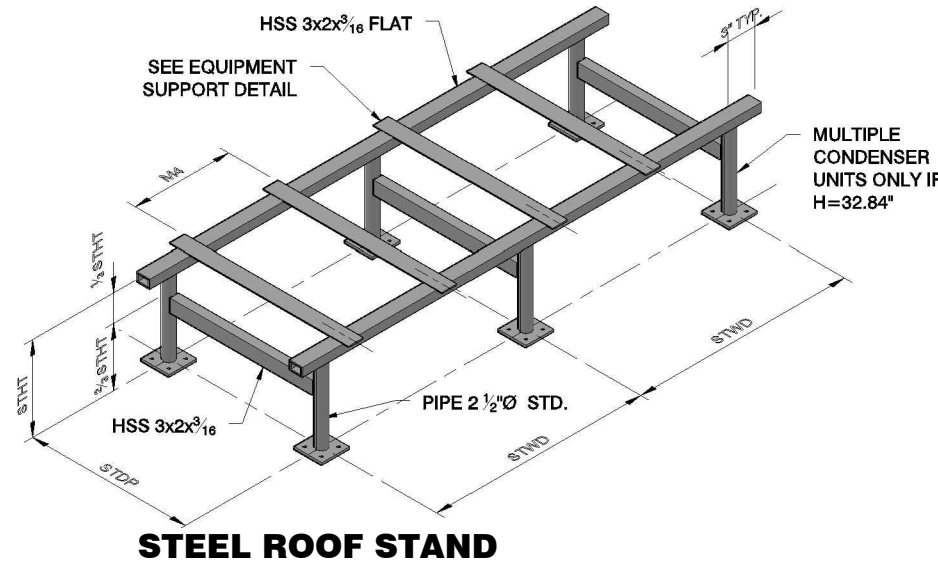
**ENCLOSURE FASTENERS:**

7. THE METAL SHELL FASTENERS MUST RESIST THE NEGATIVE WIND PRESSURES CAUSING TENSILE STRESS IN THE SCREWS AND PULL-OVER EFFECTS OF THE SHEET METAL.



**ROOF-MOUNT CONFIGURATION**

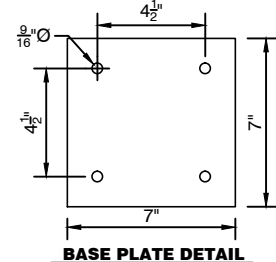
SCALE: NTS



**STEEL ROOF STAND**

SCALE: NTS

ROOF STAND STRENGTH LIMITS		
LIMIT TYPE	AMOUNT	UNITS
MAX SHEAR AT POST BASE	1.100	KIP
MAX PULLOUT AT POST BASE	3.400	KIP
MAX MOMENT AT POST BASE	16.70	KIP*IN
MAX MOMENT AT CROSS BRACE	16.71	KIP*IN



**ROOF STAND NOTES:**

1. ROOF STAND IS DESIGNED AND VERIFIED FOR THE FORCES DESCRIBED IN THIS DOCUMENT AS SUMMARIZED IN THE ENGINEERING CALCULATIONS INCLUDED.
2. STHT = STAND HEIGHT = MIN 18", MAX 30".
3. STWP = STAND POST SPACING = 32" MIN, 40" MAX.
4. STDP = STAND DEPTH = 25" MIN, 30" MAX.
5. EQUIPMENT SUPPORT AND FASTENERS TO STAND TOP RAIL ARE DEFINED IN SEPARATE DETAIL.
6. AC UNIT MUST BE CENTERED ON SUPPORT.
7. 3/8" BASE PLATE IS ANCHORED TO CONCRETE SLAB W/ 1/2" Ø ADHESIVE ANCHORS (HILTI HIT-HY 200+HAS) WITH MIN. 3" EMBED. OF GALV HAS RODS IN CONCRETE. ANCHOR GROUP CAPACITY COMBINED TENSION = 3400 LBS, SHEAR = 1100 LBS, AND MOMENT 16700 IN\*lbs.
8. IF NO ROOF SLAB, BASE PLATES SHALL BE ANCHORED TO STEEL ROOF FRAMING (DESIGNED BY OTHERS FOR THESE LOADS) WITH 3/8" Ø A307 BOLTS W/ 7/16" Ø HOLES IN BASE PLATES..

**STEEL FABRICATION NOTES:**

- ALL MATERIAL IS STEEL WITH MIN  $F_y = 35$  KSI.
- ALL JOINTS SHALL BE WELDED CONTINUOUS ALL AROUND W/ 3/16" FILLET.

**OTHER NOTES:**

- EQUIPMENT SUPPORT IS NOT PART OF ROOF STAND.
- MIN NUMBER OF POSTS IS 4. ONLY FOR UNITS W/ H=32.84", STANDS W/ 6 POSTS OR MORE MAY BE USED AS INDICATED IN SKETCH. FOR UNITS W/ H=54.34", USE ONE STAND PER CONDENSER.
- 1" ± NON-METALLIC NON-SHRINK GROUT MAY BE USED UNDER THE BASE PLATES.

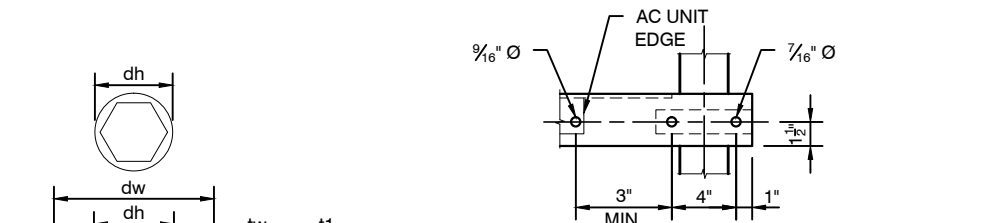
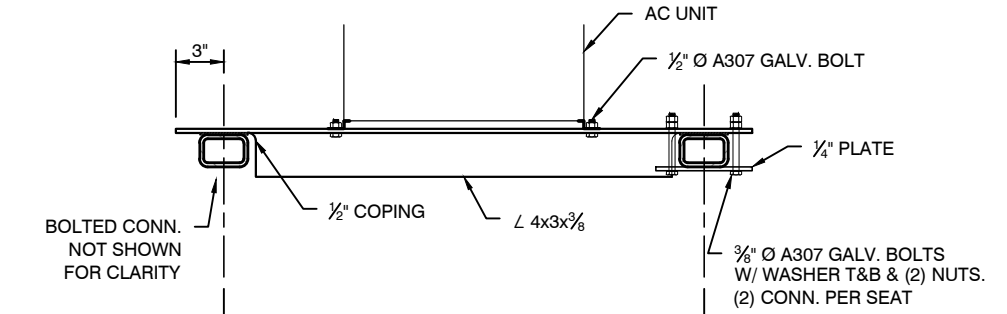
**ENGINEERING CONFORMANCE ANALYSIS:**

THE TABLE BELOW SHOWS DIMENSIONS, MIN STAND DEPTH, & SHELL ENCLOSURE SCREWS FOR SOME MODELS OF LG ELECTRONICS USA HVAC OUTDOOR EQUIPMENT THAT MEET THE FOLLOWING ANALYSIS:

- ROOF STAND STRENGTH: POST AND CROSS-BRACE STRENGTH TO RESIST UNIT WEIGHT AND WIND LOAD LATERAL AND VERTICAL SURFACES
- STAND POST ANCHORS: PULLOUT AND SHEAR DUE TO OVERTURNING AND SLIDING FORCE IS WITHIN REQUIREMENTS
- EQUIPMENT METAL COVER FASTENERS: MIN NUMBER AND SIZE

MODEL #	CONDENSER DIMENSIONS						ROOF STAND DIMS: STDP MIN (IN)	SHELL SCREWS ON LONG SIDE, QTY. & SIZE	STAND STRENGTH			METAL SHELL
	W	D	H	M1	M4	Wt			ANCHOR SHEAR	UPLIFT	BRACE MOMENT	
	DESIGN CHECK W/ NOM/REQ'D = 1.00 = OK											
LMU30CHV	37.41	13.00	32.84	14.38	24.41	136.7	25	12, #10	0.38	0.43	0.50	0.82
LMU36CHV	37.41	13.00	32.84	14.38	24.41	136.7	25	12, #10	0.38	0.43	0.50	0.82
LUU187HV	37.41	13.00	32.84	14.38	24.41	132.3	25	12, #10	0.38	0.43	0.50	0.82
LUU247HV	37.41	13.00	32.84	14.38	24.41	132.3	25	12, #10	0.38	0.43	0.50	0.82
LMU480HV	37.41	13.00	54.34	14.38	24.41	213.8	25	18, #10	0.63	0.85	0.83	0.90
LMU540HV	37.41	13.00	54.34	14.38	24.41	213.8	25	18, #10	0.63	0.85	0.83	0.90
LMU600HV	37.41	13.00	54.34	14.38	24.41	213.8	25	18, #10	0.63	0.85	0.83	0.90
LUU367HV	37.41	13.00	54.34	14.38	24.41	202.8	25	18, #10	0.63	0.85	0.83	0.90
LUU427HV	37.41	13.00	54.34	14.38	24.41	202.8	25	18, #10	0.63	0.85	0.83	0.90
ARUN038GSS4	37.41	13.00	54.34	14.38	24.41	207	25	18, #10	0.63	0.85	0.83	0.90
ARUN048GSS4	37.41	13.00	54.34	14.38	24.41	207	25	18, #10	0.63	0.85	0.83	0.90
ARUN054GSS4	37.41	13.00	54.34	14.38	24.41	207	25	18, #10	0.63	0.85	0.83	0.90

NOTE: THE STAND DIMENSIONS ARE MINIMUMS. STAND MAY BE BUILT TO SUPPORT MORE THAN ONE CONDENSER UNIT AS OUTLINED IN THE LG ELECTRONICS USA INSTALLATION MANUAL.



**EQUIPMENT SUPPORT DETAIL**

SCALE: NTS

ENCLOSURE FASTENERS		
DESCRIPTION	SIZE	UNITS
SCREW SIZE (d)	#10	
INTEGRAL WASHER SIZE (dw)	0.50	IN
THICKNESS OF SHEET METAL (t1)	0.043	IN
MIN. THICKNESS OF FRAME (t2)	0.07	IN
DEPTH OF PENETRATION	0.25	IN
SCREW YIELD STRENGTH	55	KSI
ALLOWABLE TENSILE STRENGTH/SCREW	321	LBS
ALLOWABLE PULLOVER STRENGTH/SCREW	371	LBS
ALLOWABLE PULL-OUT STRENGTH/SCREW	170	LBS



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 Certificate of Authorization  
 # 31626

DRAWING TITLE  
**37-13-R-105 INFORMATION & DIAGRAMS**

PROJECT TITLE  
**LG ELECTRONICS USA HVAC  
 OUTDOOR CONDENSING UNIT  
 ROOF MOUNT CONFIGURATION**

NO.	DATE	BY	DESCRIPTION

SCALE: NTS      DATE: 11/02/16  
 DRAWN BY: JDP      PROJECT MGR: PCP  
 PROJECT NO.: 160387      FLAT FILE:  
 DRAWING NO.: **37-13-R-105**  
 SHEET **1** OF **2**

# ENGINEERING CALCULATION DETAIL SHEET

Outdoor Condensor Units on Roof Stand - Suitability Verification  
 Designed by: Paul C. Perrin, PE, SE

DESIGN METHODOLOGY: ASD

**OBJECTIVE:**

Determine Wind Load on AC unit mounted on roof stand using ASCE 7 (2010), Section 29.5. Confirm stability, roof stand strength, anchor configuration and strength, and equipment envelope fastening.

WIND LOAD: (See also "Wind Design Requirements" on Drawing 1)

Vult = 186 mph (FBC 2014 1620.2) for Miami-Dade, Risk Category IV

From "29.3 Velocity Pressure"

$qz = 0.00256 * Kz * Kzt * Kd * V^2 = 105 \text{ psf}$  (Eq. 29.3-1)

From "29.5 Design Wind Loads - Other Structures"

$F = qz * (GCr) * Af$  (Eq. 29.5-1)

$F_{\text{vertical}} = 105 \text{ psf} * (1.50) * Af = 157.8 \text{ psf} * \text{Area (ft}^2)$

$F_{\text{lateral}} = 105 \text{ psf} * (3.10) * Af = 326.2 \text{ psf} * \text{Area (ft}^2)$

Example AC Unit:

Use LUU187HV in Table w/ dims (W, D, H, Wt) = ( 37.41", 13", 32.84", 132.3 lbs)

WIND LOAD FORCES:

Top Area =  $13" * 37.41" / (144 \text{ in}^2/\text{ft}^2) = 3.38 \text{ sf}$   
 $Fw_{\text{vertical}} (Fw_{\text{vert}}) = 157.8 \text{ psf} * 3.38 \text{ sf} = 533 \text{ lbs (unfactored)}$

Long side Area =  $37.41" * 32.84" / (144 \text{ in}^2/\text{ft}^2) = 8.53 \text{ sf}$   
 $Fw_{\text{lateral}} (Fw_{\text{lat}}) = 326.2 \text{ psf} * 8.53 \text{ sf} = 2783 \text{ lbs (unfactored)}$

LOAD COMBINATIONS:

0.67D + 0.78W for overturning FBC 1605.3.2 Eq. 16-18  
 0.6D + 0.6W for sliding and anchors FBC 1605.3.1 Eq. 16-15

CALCULATE REACTION FORCES ON ROOF STAND:

Shear V1 =  $0.6 * Fw_{\text{lat}} / 4 \text{ posts} = 0.6 * 2783 \text{ #} / 4 = 417 \text{ lbs}$

Pull-up R1 =  $[ 0.6 * Fw_{\text{lat}} * b + (0.6 * Fw_{\text{vert}} - 0.6 * Wt) * (a+3") ] / (2 * a+3") / 2 \text{ posts}$   
 $= [ 0.6 * 2783 \text{ #} * (30" + 32.84"/2) + (0.6 * 533 \text{ #} - 0.6 * 132.3 \text{ #}) * (12.5"/2 + 3") ] / (12.5" + 3") / 2$   
 = 1.451 kips

Moment MB =  $V1 * ST-U = 417 \text{ #} * 20" = 8.348 \text{ kip-in}$

NOMINAL STRENGTH OF ROOF STAND:

All limits are based on posts at min. depth of 25", max. height of 30", and max. spacing of 40".

Limits: Shear at base, Uplift at one post, Moment on frame

Given:

- (4) anchors per base with allowable max pull-up of 3400 lbs, allowable max shear of 1100 lbs and allowable max moment of 16.70 kip-in per anchor group, (1/2" diameter adhesive anchor with 3" embedment in min 3000 psi concrete).
- All welds 3/16" fillet. All materials steel with min Fy = 35 ksi.

Posts are 2.5" Ø standard pipe.

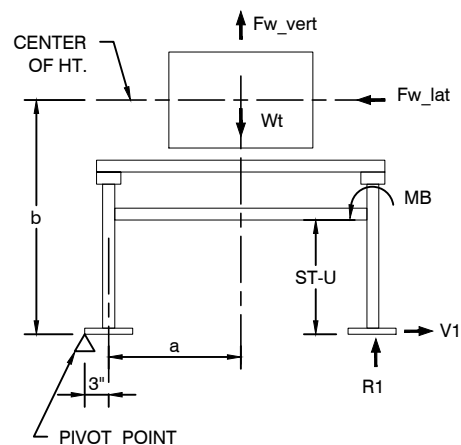
Cross brace is HSS 3 x 2 x 3/16"

Limits per post:

Max shear = min(pipe shear, anchor shear)  
 $= \min(0.6 * 35 \text{ ksi} * 1.61 * \text{in}^2 / 1.67, 1.100 \text{ kips})$   
 = 1.100 kips

Max uplift at one post = anchor pull-up capacity = 3400 lbs = 3.400 kips

Max moment at brace  
 $= \min(\text{brace flexural strength, weld strength, post flexural strength})$   
 $= \min(46 \text{ ksi} * 1.18 \text{ in}^3 / 1.67, 2.78 \text{ kip-in} * 2" * 3", 35 \text{ ksi} * 1.01 \text{ in}^3 / 1.67)$   
 $= \min(32.5 \text{ kip-in, } 16.7 \text{ kip-in, } 21.2 \text{ kip-in})$   
 = 16.7 kip-in



SINCE THIS DESIGN IS BASED ON WIND PRESSURE, qz, THIS DESIGN IS ALSO SUITABLE FOR THE FOLLOWING CASES:

- MIAMI DADE WIND SPEED = 186 MPH, RISK CATEGORY IV, EXPOSURE CATEGORY C, HEIGHT UP TO 124 FT.
- MIAMI DADE WIND SPEED = 186 MPH, RISK CATEGORY II, EXPOSURE CATEGORY D, HEIGHT UP TO 125 FT.
- BROWARD WIND SPEED = 180 MPH, RISK CATEGORY IV, EXPOSURE CATEGORY D, HEIGHT UP TO 93 FT.

DESIGN METHODOLOGY: ASD

VERIFY ANCHOR SHEAR RESISTANCE TO SLIDING:

Use Load Combination FBC 1605.3.1 Eq. 16-15  
 $0.6D + 0.6W = 0.6 * Fw_{\text{lat}} = 0.6 * 2783 \text{ #} = 1670 \text{ lbs}$   
 Shear per post =  $1670 \text{ #} / 4 = 417 \text{ lbs}$   
 Fsliding nominal = 1.100 kips  
 Since 1.100 kips > 0.417 kips

Resistance to Sliding Checks OK.

CHECK OVERTURNING ANCHOR PULLOUT/UPLIFT RESISTANCE:

Use Load Combination FBC 1605.3.1 Eq. 16-15  
 $0.6D + 0.6W$   
 On one post  
 Pull-up R1 = 1.451 kips  
 Max uplift at one post = 3.400 kips  
 Since 3.400 kips > 1.451 kips

Anchor Resistance to Overturning Checks OK.

CHECK BRACE RESISTANCE TO MOMENT:

Use worst case on one post  
 Moment at brace MB = 8.348 kip-in per post  
 Max moment at brace = 16.7 kip-in  
 Since 16.7 kip-in > 8.348 kip-in

Moment at Stand Brace Checks OK.

CHECK SHEET METAL ENVELOPE FASTENER RESISTANCE:

Analysis based on AISI S100-2007 "Cold Formed Steel Structural Members" Section E4:Screw Connections  
 Use Load Combination FBC 1605.3.1 Eq. 16-15  
 $0.6D + 0.6W$   
 On long side worst case  
 $0.60 * Fw_{\text{lat}} = 0.60 * 2783 \text{ #} = 1670 \text{ lbs}$

Resistance to the metal shell pull-off is the minimum of the tensile strength of the screw and the pull-over strength of the sheet metal.

Inputs:

#10 screw, d = 0.19" with integral 0.5"-diameter washer  
 Thickness of metal shell, t1 = 0.043" (18 gauge)  
 Depth of penetration of screw into frame, tc = 0.25"  
 Strength of screw, Fu1 = 55 ksi

Based on the above data:

Allowable tensile of the screw,  $Pts/\Omega = 321 \text{ lbs per screw (where } \Omega = 3.0)$   
 Allowable Pull-out strength,  $Pnot/\Omega = 170 \text{ lbs per screw}$   
 Allowable Pull-over strength,  $Pnov/\Omega = 371 \text{ lbs per screw}$   
 Therefore the min number of screws per long side =  $1670 \text{ #} / 170 \text{ #/screw} = 9.82 \text{ screws}$   
 Rounds up to min 10 screws per side, use 12 screws for symmetry.

Anchor Resistance to Metal Enclosure Pull-Off Checks OK.

VERIFY STRENGTH OF SUPPORT BARS AND CONNECTIONS:

Use Load Combination  
 $0.67 D + 0.78 W$   
 Max uplift on one side of AC Unit at mounting anchors:  
 $F_{M1} = (0.78 * Fw_{\text{lat}} * H/2) / (2 * M1) + (0.78 * Fw_{\text{vert}} - 0.67 * Wt) / 4 =$   
 $F_{M1} = (0.78 * 2.78 \text{ kips} * 32.84 \text{ in} / 2) / (2 * 14.375 \text{ in}) + (0.78 * 0.53 \text{ kips} - 0.67 * 0.132 \text{ kips}) / 4$   
 $F_{M1} = 1.321 \text{ kips}$   
 Allowable tensile capacity of bolt = 4.42 kips > 1.321 kips  
 Bolt Resistance at Mounting Anchor Checks OK

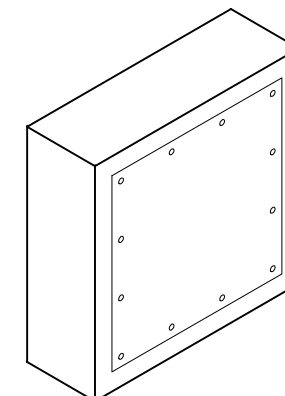
Max uplift on one side of AC Unit at side support HSS:  
 $F_{STDP} = (0.78 * Fw_{\text{lat}} * H/2) / (2 * STDP) + (0.78 * Fw_{\text{vert}} - 0.67 * Wt) / 4 =$   
 $F_{STDP} = (0.78 * 2.78 \text{ kips} * 32.84 \text{ in} / 2) / (2 * 30 \text{ in}) + (0.78 * 0.53 \text{ kips} - 0.67 * 0.132 \text{ kips}) / 4$   
 $F_{STDP} = 0.676 \text{ kips}$   
 Allowable tensile capacity of 2 bolts =  $2 * 2.49 \text{ kips} = 4.97 \text{ kips} > 0.676 \text{ kips}$   
 Bolt Resistance at Side Supports Checks OK

Max moment in Support Angle:  
 $F_{M1} * (STDP - M1) / 2 = 1.321 \text{ kips} * (30 \text{ in} - 14.375 \text{ in}) / 2 = 10.324 \text{ kip-in}$   
 $Sx * Fy / \Omega = 1.44 \text{ in}^3 * 36 \text{ ksi} / 1.67 = 31.042 \text{ kip-in} > 10.324 \text{ kip-in}$   
 Support Angle Flexural Capacity Checks OK

Max moment in Side HSS:  
 $F_{STDP} * (STWD - M4) / 2 = 0.676 \text{ kips} * (40 \text{ in} - 24.41 \text{ in}) / 2 = 5.269 \text{ kip-in}$   
 $Sy * Fy / \Omega = 0.932 \text{ in}^3 * 46 \text{ ksi} / 1.67 = 25.672 \text{ kip-in} > 5.269 \text{ kip-in}$   
 Side HSS Flexural Capacity Checks OK

THE CALCULATIONS ON THE DRAWING ARE REPRESENTATIVE OF THE FOLLOWING LG ELECTRONICS OUTDOOR CONDENSING UNITS:

LMU30CHV
LMU36CHV
LUU187HV
LUU247HV
LMU480HV
LMU540HV
LMU600HV
LUU367HV
LUU427HV
ARUN038GSS4
ARUN048GSS4
ARUN054GSS4



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DRAWING TITLE  
 PROJECT TITLE  
**37-13-R-105 CALCULATIONS**  
**LG ELECTRONICS USA HVAC**  
**OUTDOOR CONDENSING UNIT**  
**ROOF MOUNT CONFIGURATION**

REVISIONS		SCALE	DATE
NO.	DESCRIPTION	BY	

DRAWING NO.  
**37-13-R-105**

SHEET 2 OF 2

**PAUL C. PERRIN**  
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 PROFESSIONAL ENGINEER