

CODES:

FLORIDA BUILDING CODE 2014, 5TH EDITION
ASCE STANDARD 7-2010
MIAMI DADE WIND SPEED = 186 MPH

WIND DESIGN REQUIREMENTS:

ULTIMATE DESIGN WIND SPEED, V_{ult} (3 sec. gust)	186 mph
NOMINAL DESIGN WIND SPEED, V_{asd}	144 mph
RISK CATEGORY	IV
HEIGHT TO CENTROID	15 FT max.
EXPOSURE CATEGORY	D
ENCLOSURE CATEGORY	N/A
EFFECTIVE WIND AREA	N/A
INTERNAL PRESSURE COEFFICIENT GCP_i	N/A
DIRECTIONALITY FACTOR K_d	0.90
TOPOGRAPHIC FACTOR K_{zt}	1.00
GUST EFFECT FACTOR	N/A

WIND LOAD METHOD:

VELOCITY PRESSURE:
based on ASCE 7-10, Eq. 29.3-1
 $q_z = 0.00256 K_z K_{zt} K_d V^2$ psf
 $K_z = 1.03$
 $V = V_{ult}$
 $q_z = 82.1$ psf

WIND PRESSURES:
based on ASCE 7-10 Eq. 29.5.1 & FBC 1620.6
 $F = q_h GC_r Af$ psf Eq 29.5-2
 $GC_r = 1.1$ FOR LATERAL FORCES
 $GC_r = 1.0$ FOR VERTICAL FORCES

LOAD COMBINATIONS:

- POSITIVE VERTICAL FORCE: $1.0D + 0.6W$ [FBC 1605.3.1 EQ. 16-12]
- SLIDING & ANCHOR PULLOUT: $0.6D + 0.6W$ [FBC 1605.3.1 EQ. 16-15]
- OVERTURNING: $0.67D + 0.78W$ [FBC 1605.3.2 EQ. 16-18]

GENERAL NOTES:

- THIS ENGINEERING REPORT DOCUMENTS THE ANALYSIS OF AC EQUIPMENT MOUNTED ON A CONCRETE FOUNDATION PAD AND THE ASSOCIATED ANCHORING SYSTEMS TO RESIST DEAD WEIGHT AND WIND LOAD FORCES.
- THE ANALYSIS CONFORMS TO THE REQUIREMENTS OF THE FLORIDA BUILDING CODE 2014 AND ASCE 7-2010, FOR USE WITHIN & OUTSIDE HVHZ.
- THE AC UNIT IS MOUNTED ON A CONCRETE FOUNDATION PAD. THE CONCRETE FOUNDATION PAD SHALL BE MIN 8" THICK AT ANCHOR LOCATIONS.
- THE ANCHORAGE IS DESIGNED AND VERIFIED BY STRUCTURAL ANALYSIS BY THIS ENGINEER.
- ALTERNATE DESIGNS FOR SUPPORTS WITHIN 15' OF GROUND LEVEL, THAT ARE DESIGNED TO RESIST THE ABOVE WIND LOADS MAY BE USED AT THE CONTRACTOR'S OPTION. FOR ALTERNATE DESIGNS FOR SUPPORTS WITHIN 15' OF GROUND LEVEL, PROVIDE DETAILS AND CALCULATIONS SIMILAR TO THIS SHEET AND DETAILED CALCULATIONS ON SHEET 2, STAMPED BY A PROFESSIONAL ENGINEER REGISTERED IN THE STATE OF FLORIDA.
- THE CONTRACTOR IS RESPONSIBLE FOR SAFETY, INSTALLATION, AND SPECIAL INSPECTIONS & TESTS PER FBC CHAPTER 17.

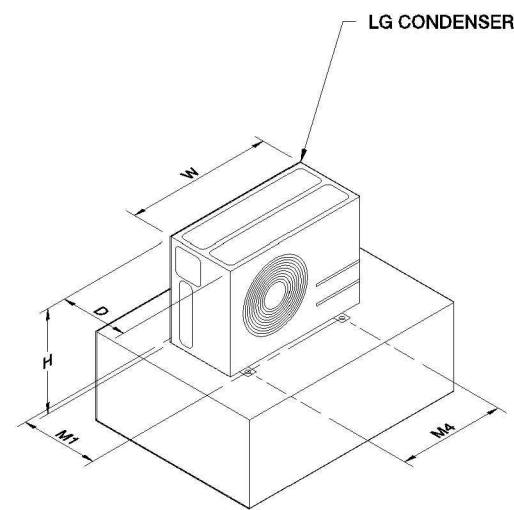
CALCULATIONS: SEE DETAILED CALCULATIONS ON SHEET 2.

WIND LATERAL AND VERTICAL FORCES:

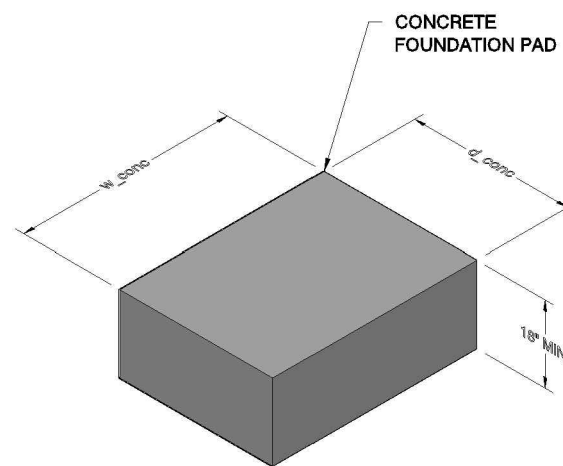
- THE WIND LOAD ACTING NORMAL TO THE LARGE VERTICAL SIDE OF THE AC UNIT IS USED FOR WORST CASE SHEAR.
- THE WIND LOAD ACTING ON THE TOP OF THE UNIT UPWARD AND THE HORIZONTAL WIND LOAD ARE USED TO CALCULATE UPLIFT AND MOMENT.
- THESE FORCES MUST BE RESISTED BY THE SHEAR AND TENSILE STRENGTHS OF THE ANCHORS HOLDING THE UNIT TO THE CONCRETE FOUNDATION. THE ANCHORAGES & MOUNTING ARE VERIFIED BY THIS ENGINEER TO BE WITHIN THE ALLOWABLE STRENGTHS OF ITS ELEMENTS AND CONNECTIONS.

ENCLOSURE FASTENERS:

- THE METAL SHELL FASTENERS MUST RESIST THE NEGATIVE WIND PRESSURES CAUSING TENSILE STRESS IN THE SCREWS AND PULL-OVER EFFECTS OF THE SHEET METAL.



GROUND MOUNT CONFIGURATION



CONCRETE PAD W/ TURNDOWN EDGE

CONCRETE FOUNDATION PAD STRENGTH LIMITS		
LIMIT TYPE	AMOUNT	UNITS
MAX SHEAR AT ANCHOR	0.200	KIP
MAX PULLOUT AT ANCHOR	0.600	KIP

FOUNDATION NOTES:

- FOUNDATION IS DESIGNED AND VERIFIED FOR THE FORCES DESCRIBED IN THIS DOCUMENT AS SUMMARIZED IN THE ENGINEERING CALCULATIONS INCLUDED.
- t_{conc} = FOUNDATION SLAB THICKNESS = 8" MIN.
- FOUNDATION HEIGHT AT EDGES = 18" MIN.
- FOUNDATION SHALL EXTEND MIN. 12" BELOW GROUND.
- w_{conc} = FOUNDATION WIDTH = 44" MIN, 72" MAX.
- d_{conc} = FOUNDATION DEPTH = 36" MIN, 72" MAX.
- TOP OF FOUNDATION PAD SHALL BE MIN. 4" ABOVE ADJACENT GRADE.
- AC UNIT MUST BE CENTERED ON FOUNDATION.
- AC UNIT IS ANCHORED TO CONCRETE SLAB W/ GALV 1/4" Ø HILTI KWIK BOLT 3 ANCHORS WITH MIN. 2" EMBED. IN CONCRETE. EACH ANCHOR CAPACITY IS COMBINED TENSION = 600 LBS AND SHEAR = 200 LBS.
- MIN. REINFORCEMENT SHALL BE ONE LAYER OF #4 BARS @ 14" EACH WAY, CENTERED IN THE CONCRETE.
- FOUNDATION SUBGRADE SHALL BE COMPACTED TO PROVIDE MIN. 1200 PSF ALLOWABLE BEARING PRESSURE.

OTHER NOTES:

- 1"± NON-METALLIC NON-SHRINK GROUT MAY BE USED UNDER THE MOUNTING PLATES.

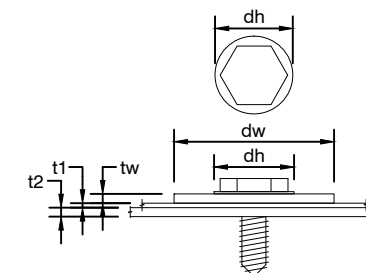
ENGINEERING CONFORMANCE ANALYSIS:

THE TABLE BELOW SHOWS DIMENSIONS, MIN FOUNDATION DEPTH & WIDTH, AND SHELL ENCLOSURE SCREWS FOR SOME MODELS OF LG ELECTRONICS USA HVAC OUTDOOR EQUIPMENT THAT MEET THE FOLLOWING ANALYSIS:

- FOUNDATION STRENGTH: STRENGTH TO RESIST UNIT WEIGHT AND WIND LOADS ON LATERAL AND VERTICAL SURFACES
- ANCHORS: PULLOUT AND SHEAR DUE TO OVERTURNING AND SLIDING FORCE IS WITHIN REQUIREMENTS
- EQUIPMENT METAL COVER FASTENERS: MIN NUMBER AND SIZE

MODEL #	CONDENSER DIMENSIONS						CONCRETE PAD		SHELL SCREWS	ANCHOR STRENGTH		METAL SHELL
	W	D	H	M1	M4	Wt	MIN d_{conc}	MIN w_{conc}		ON LONG SIDE, QTY. & SIZE	SHEAR	
LSU240HLV	34.25	12.63	31.50	14.19	21.50	125	36	44	8, #10	0.51	0.56	0.30
LSU300HLV	34.25	12.63	31.50	14.19	21.50	125	36	44	8, #10	0.51	0.56	0.30
LSU360HLV	34.25	12.63	31.50	14.19	21.50	125	36	44	8, #10	0.51	0.56	0.30
LAU180HYV1	34.25	12.63	31.50	14.19	21.50	132	36	44	8, #10	0.51	0.56	0.30
LSU180HSV4	34.25	12.63	31.50	14.19	21.50	120	36	44	8, #10	0.51	0.56	0.30
LAU240HSV2	34.25	12.63	31.50	14.19	21.50	132	36	44	8, #10	0.51	0.56	0.30
LAU240HYV1	34.25	12.63	31.50	14.19	21.50	132	36	44	8, #10	0.51	0.56	0.30
LAU240HSV3	34.25	12.63	31.50	14.19	21.50	128	36	44	8, #10	0.51	0.56	0.30
LSU240HSV3	34.25	12.63	31.50	14.19	21.50	128	36	44	8, #10	0.51	0.56	0.30
LSU243HLV	34.25	12.63	31.50	14.19	21.50	128	36	44	8, #10	0.51	0.56	0.30
LSU307HV3	34.25	12.63	31.50	14.19	21.50	128	36	44	8, #10	0.51	0.56	0.30
LSU360HV3	34.25	12.63	31.50	14.19	21.50	128	36	44	8, #10	0.51	0.56	0.30
LSU240HEV1	34.25	12.63	25.81	13.38	21.50	95	36	44	8, #10	0.42	0.40	0.25
LMU18CHV	34.25	12.63	25.78	13.38	21.50	99	36	44	8, #10	0.42	0.40	0.25
LMU24CHV	34.25	12.63	25.78	13.38	21.50	99	36	44	8, #10	0.42	0.40	0.25

NOTE: THE CONCRETE PAD DIMENSIONS ARE MINIMUMS. CONCRETE PAD MAY BE BUILT TO SUPPORT MORE THAN ONE CONDENSER UNIT AS OUTLINED IN THE LG ELECTRONICS USA INSTALLATION MANUAL.



ENCLOSURE FASTENERS		
DESCRIPTION	SIZE	UNITS
SCREW SIZE (d)	#10	
INTEGRAL WASHER SIZE (dw)	0.50	IN
THICKNESS OF SHEET METAL (t1)	0.043	IN
MIN. THICKNESS OF FRAME (t2)	0.07	IN
DEPTH OF PENETRATION	0.25	IN
SCREW YIELD STRENGTH	55	KSI
ALLOWABLE TENSILE STRENGTH/SCREW	321	LBS
ALLOWABLE PULLOVER STRENGTH/SCREW	371	LBS
ALLOWABLE PULL-OUT STRENGTH/SCREW	170	LBS



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DRAWING TITLE
34-12-G-82 INFORMATION & DIAGRAMS
 PROJECT TITLE
**LG ELECTRONICS USA HVAC
 OUTDOOR CONDENSING UNIT
 GROUND MOUNT CONFIGURATION**

NO.	DATE	BY	DESCRIPTION

SCALE: NTS
 DATE: 10/28/16
 DRAWN BY: JDP
 PROJECT MGR: PCP
 PROJECT NO.: 160387
 FLAT FILE:
 DRAWING NO.:
34-12-G-82
 SHEET **1** OF **2**

ENGINEERING CALCULATION DETAIL SHEET

Outdoor Condensor Units on Concrete Pad - Suitability Verification
 Designed by: Paul C. Perrin, PE, SE

DESIGN METHODOLOGY: ASD

OBJECTIVE:

Determine Wind Load on AC unit mounted on concrete foundation using ASCE 7 (2010), Section 29.5. Confirm stability, anchor configuration and strength, and equipment envelope fastening.

WIND LOAD: (See also "Wind Design Requirements" on Drawing 1)

Vult = 186 mph (FBC 2014 1620.2) for Miami-Dade, Risk Category IV

From "29.3 Velocity Pressure"

$$qz = 0.00256 * Kz * Kzt * Kd * V^2 = 82.1 \text{ psf} \quad (\text{Eq. 29.3-1})$$

From "29.5 Design Wind Loads - Other Structures"

$$F = qz * (GCr) * Af \quad (\text{Eq. 29.5-1})$$

$$F_{\text{vertical}} = 82.1 \text{ psf} * (1.0) * Af = 82.1 \text{ psf} * \text{Area} \text{ (ft}^2\text{)}$$

$$F_{\text{lateral}} = 82.1 \text{ psf} * (1.1) * Af = 90.3 \text{ psf} * \text{Area} \text{ (ft}^2\text{)}$$

Example AC Unit:

Use LSU180HSV4 in Table w/ dims (W, D, H, Wt) = (34.25", 12.625", 31.5", 120.2 lbs)

WIND LOAD FORCES:

$$\begin{aligned} \text{Top Area} &= 12.625" * 34.25" / (144 \text{ in}^2/\text{ft}^2) = 3.00 \text{ sf} \\ F_{\text{w vertical}} &= 82.1 \text{ psf} * 3.00 \text{ sf} = 247 \text{ lbs (unfactored)} \end{aligned}$$

$$\begin{aligned} \text{Long side Area} &= 34.25" * 31.5" / (144 \text{ in}^2/\text{ft}^2) = 7.49 \text{ sf} \\ F_{\text{w lateral}} &= 90.3 \text{ psf} * 7.49 \text{ sf} = 677 \text{ lbs (unfactored)} \end{aligned}$$

LOAD COMBINATIONS:

$$\begin{aligned} 0.67D + 0.78W \text{ for overturning} & \quad \text{FBC 1605.3.2 Eq. 16-18} \\ 0.6D + 0.6W \text{ for sliding and anchors} & \quad \text{FBC 1605.3.1 Eq. 16-15} \end{aligned}$$

CALCULATE REACTION FORCES ON CONCRETE FOUNDATION:

$$\begin{aligned} \text{Shear } V_1 &= 0.6 * F_{\text{w lateral}} / 4 \text{ anchors} = 0.6 * 677 \text{ \#} / 4 = 101 \text{ lbs} \\ \text{Pull-up } R_1 &= [0.78 * F_{\text{w lateral}} * H/2 + (0.78 * F_{\text{w vertical}} - 0.67 * Wt) * (M1/2)] / (M1) / 2 \text{ legs} \\ &= [0.78 * 677 \text{ \#} * (31.5"/2) + (0.78 * 247 \text{ \#} - 0.67 * 120.2 \text{ \#}) * (13.38"/2)] / (13.38") / 2 \\ &= 0.339 \text{ kips} \end{aligned}$$

SOIL BEARING PRESSURE AT CONCRETE FOUNDATION:

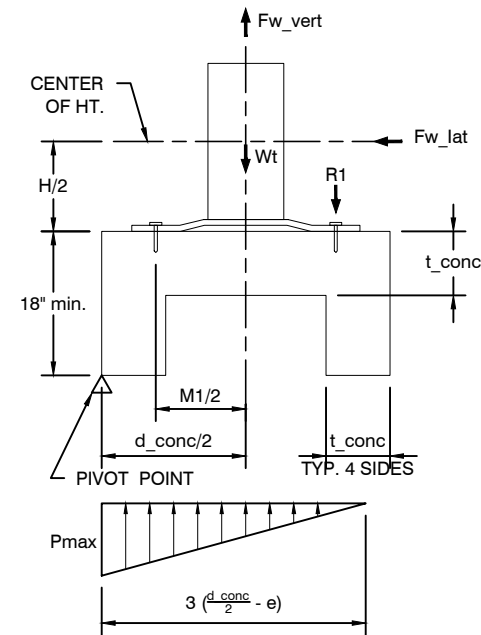
$$\begin{aligned} W_{\text{t conc}} &= 150 \text{ pcf} * \{t_{\text{conc}} * w_{\text{conc}} * d_{\text{conc}} + (18" - t_{\text{conc}}) * 2 * t_{\text{conc}} * [w_{\text{conc}} + (d_{\text{conc}} - 2 * t_{\text{conc}})]\} \\ &= 150 \text{ pcf} * \{8" * 44" * 36" + (18" - 8") * 2 * 8" * [44" + (36" - 2 * 8")]\} \\ &= 1.99 \text{ kips} \end{aligned}$$

$$\begin{aligned} P &= 0.67 * (Wt + W_{\text{t conc}}) - 0.78 * F_{\text{w vertical}} \\ &= 0.67 * (0.120 \text{ kip} + 1.99 \text{ kip}) - 0.78 * 247 \text{ \#} \\ &= 1.221 \text{ kip} \end{aligned}$$

$$\begin{aligned} M_{\text{ot}} &= 0.78 * F_{\text{w lateral}} * (18" + H/2) \\ &= 0.78 * 677 \text{ \#} * (18" + 31.5"/2) \\ &= 17.812 \text{ kip*in} \end{aligned}$$

$$e = M_{\text{ot}} / P = 17.812 \text{ kip*in} / 1.221 \text{ kips} = 14.591"$$

$$\begin{aligned} \text{If } e = 14.591" > d_{\text{conc}}/6 = 6.00" \\ \text{then } P_{\text{max}} &= 2P / \{3 * w_{\text{conc}} * [(d_{\text{conc}}/2) - e]\} \\ &= 2 * 1.221 \text{ kip} / \{3 * 44" * [(36"/2) - 14.591"]\} \\ &= 781 \text{ psf} \end{aligned}$$



DESIGN METHODOLOGY: ASD

VERIFY ANCHOR SHEAR RESISTANCE TO SLIDING:

$$\begin{aligned} \text{Use Load Combination FBC 1605.3.1 Eq. 16-15} \\ 0.6D + 0.6W = 0.6 * F_{\text{w lateral}} = 0.6 * 677 \text{ \#} = 406 \text{ lbs} \\ \text{Shear per anchor} = 406 \text{ \#} / 4 = 101 \text{ lbs} \\ F_{\text{sliding nominal}} = 0.200 \text{ kips} \\ \text{Since } 0.200 \text{ kips} > 0.101 \text{ kips} \end{aligned}$$

Resistance to Sliding Checks OK.

CHECK OVERTURNING ANCHOR PULLOUT/UPLIFT RESISTANCE:

$$\begin{aligned} \text{Use Load Combination FBC 1605.3.1 Eq. 16-15} \\ 0.6D + 0.6W \\ \text{On one anchor} \\ \text{Pull-up } R_1 = 0.339 \text{ kips} \\ \text{Max uplift at one anchor} = 0.600 \text{ kips} \\ \text{Since } 0.600 \text{ kips} > 0.339 \text{ kips} \end{aligned}$$

Anchor Resistance to Overturning Checks OK.

CHECK SHEET METAL ENVELOPE FASTENER RESISTANCE:

$$\begin{aligned} \text{Analysis based on AISI S100-2007 "Cold Formed Steel Structural Members" Section} \\ \text{E4: Screw Connections} \\ \text{Use Load Combination FBC 1605.3.1 Eq. 16-15} \\ 0.6D + 0.6W \\ \text{On long side worst case} \\ 0.60 * F_{\text{w lateral}} = 0.60 * 677 \text{ \#} = 406 \text{ lbs} \end{aligned}$$

Resistance to the metal shell pull-off is the minimum of the tensile strength of the screw and the pull-over strength of the sheet metal.

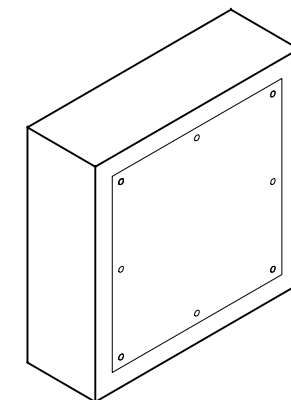
Inputs:

#10 screw, d = 0.19" with integral 0.5"-diameter washer
 Thickness of metal shell, t1 = 0.043" (18 gauge)
 Depth of penetration of screw into frame, tc = 0.25"
 Strength of screw, Fu1 = 55 ksi

Based on the above data:

Allowable tensile of the screw, Pts/Omega = 321 lbs per screw (where Omega = 3.0)
 Allowable Pull-out strength, Pnot/Omega = 170 lbs per screw
 Allowable Pull-over strength, Pnov/Omega = 371 lbs per screw
 Therefore the min number of screws per long side = 406# / 170#/screw = 2.39 screws
 Rounds up to min 3 screws per side, use 8 screws, spaced 12" O.C. minimum.

Anchor Resistance to Metal Enclosure Pull-Off Checks OK.

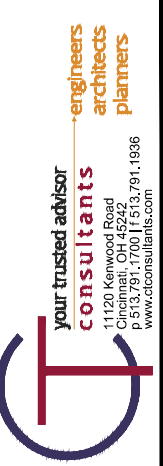


SCREW PATTERN

SCALE: NTS

THE CALCULATIONS ON THE DRAWING ARE REPRESENTATIVE OF THE FOLLOWING LG ELECTRONICS OUTDOOR CONDENSING UNITS:

LSU240HLV
LSU300HLV
LSU360HLV
LAU180HYV1
LSU180HSV4
LAU240HSV2
LAU240HYV1
LAU240HSV3
LSU240HSV3
LSU243HLV
LSU307HV3
LSU360HV3
LSU240HEV1
LMU18CHV
LMU24CHV



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34-12-G-82 CALCULATIONS
 LG ELECTRONICS USA HVAC
 OUTDOOR CONDENSING UNIT
 GROUND MOUNT CONFIGURATION

NO.	DATE	BY	DESCRIPTION	SCALE	DATE
				NTS	10/28/16
		JDP			PCP
				160387	
DRAWING NO. 34-12-G-82					
SHEET 2 OF 2					

